



Program Description I

Program Title ELLIPTIC LOWPASS FILTER DESIGN

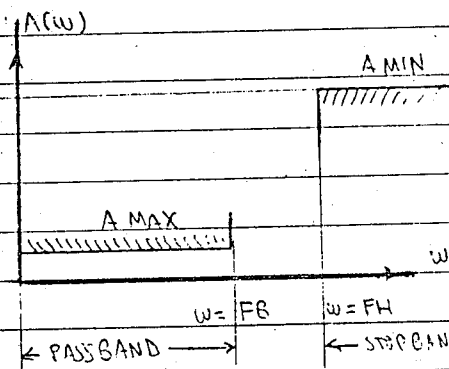
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Program Description, Equations, Variables: THIS PROGRAM IS INTENDED AS A HELP WHEN DESIGNING ELLIPTIC LOWPASS FILTERS (OR HIGHPASS, BANDPASS, BANDSTOP ONCE THEY HAVE BEEN TRANSFORMED INTO A NORMALIZED LOWPASS). THE PROGRAM CAN BE USED TO FIND THE MINIMUM DEGREE OF AN ELLIPTIC LOWPASS FILTER THAT MEETS THE

STANDARD REQUIREMENTS A_{MIN} , A_{MAX} , F_B , F_H , WHERE =



- A_{MIN} = MINIMUM STOPBAND LOSS
- A_{MAX} = MAXIMUM PASSBAND LOSS
- F_B = UPPER PASSBAND EDGE
- F_H = UPPER STOPBAND EDGE

IF THE DEGREE N IS $N \leq 30$, THE PROGRAM

ALSO FINDS THE ZEROS & POLES OF ATTENUATION

AND, USING CARD 2, CAN FIND THE LOSS AT ANY

DESIRED FREQUENCY, EITHER MANUALLY OR AUTOMATICALLY. IN THE CASE YOU PREFER AN AUTOMATIC PLOT, THERE IS A CHOICE BETWEEN LINEAR OR LOGARITHMIC SWEEP.

EQUATIONS USED ARE =

- CONSIDER THE ELLIPTIC INTEGRAL OF THE 1ST KIND $\equiv U(\phi, k) = \int_0^\phi \frac{dx}{\sqrt{1-k^2 \sin^2 x}}$

- THEN, THE COMPLETE ELLIPTIC INTEGRAL IS EXPRESSED AS:

$$K(k) = U(\pi/2, k) = \int_0^{\pi/2} \frac{dx}{\sqrt{1-k^2 \sin^2 x}}$$

AND THE COMPLEMENTARY COMPLETE ELLIPTIC INTEGRAL:

$$K'(k) = K(k'), \text{ WHERE } k' = \sqrt{1-k^2}$$

- THE ELLIPTIC SINE: $SN(u, k) = \sin \phi$

- THEN, WE COMPUTE $X_L = F_H/F_B$, $E = 10^{0.1 A_{MAX}} - 1$

$$L = \sqrt{\frac{10^{0.1 A_{MIN}} - 1}{10^{0.1 A_{MAX}} - 1}}$$

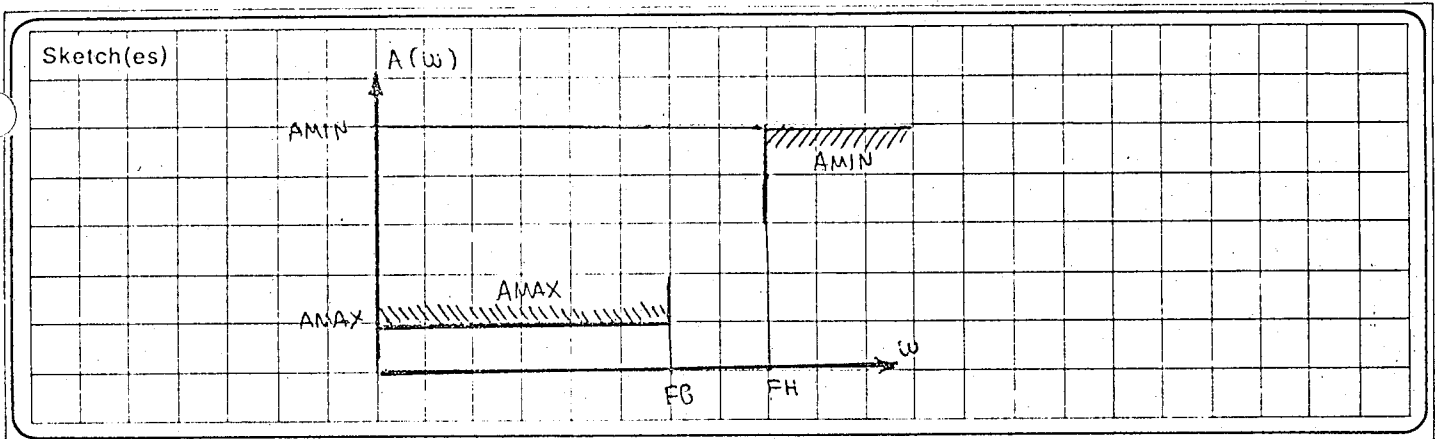
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Program Description II



Example Problem(s) NOW, LET'S SEE ALL FUNCTIONS A LITTLE CLOSER:

CARD 1 (BOTH CARDS WORKS ON RADIAN MODE)

CARD 1 DOES NOT DEPEND ON CARD 2 TO PERFORM ITS FUNCTIONS. IN FACT, CARD 2 IS ONLY FOR EVALUATING THE LOSS ONCE ZEROS & POLES HAVE BEEN COMPUTED BY CARD 1

LBLA INPUT: A_MIN [ENTER] A_MAX [ENTER] F_H [ENTER] F_B [A] → m (DEGREE)

CHARACTERISTICS

- IT TAKES ABOUT 87 SECONDS (ON THE AVERAGE)
- A_MIN, A_MAX, ... ARE USED, BUT ONLY F_B, A_MIN ARE STORED
- IT DESTROYS PREVIOUS ZEROS & POLES IN R₈, R₄

LBLB PRESS [B] (DEGREE m MUST HAVE BEEN PREVIOUSLY COMPUTED, OF COURSE)

→ (1) → XZ₁ → XP₁ (DSP 9)

→ (2) → XZ₂ → XP₂ (DSP 9)

→ (m) → XZ_m → XP_m → 0.00

WHERE m = INT(m/2)

Buttons(es)

CHARACTERISTICS

- TO BE USED ONCE m HAS BEEN COMPUTED
- ONLY IF m ≤ 30 (m ODD OR EVEN)
- IT TAKES ABOUT 1/2 × 13 SECONDS PER DEGREE
(I.E. IF DEGREE IS 2×3, THEN CALCULATION OF ZEROS & POLES WILL LAST ABOUT 40 SECONDS)
- ZEROS ARE STORED IN R₁ THROUGH R₁₅
(POLES NEED NOT BE STORED, THEY ARE FUNCTION OF ZEROS)

Reference(s)

LBLC ALLOWS REVIEWING BOTH ZEROS & POLES AT ANY TIME

PRESS [C] → (1) → XZ₁ → XP₁ (DSP 9)

→ (2) → XZ₂ → XP₂ (DSP 9)

→ (x) → XZ_x → XP_x → 0.00 (x = INT(m/2))

LBL D COMPUTES $Z(K) = \int_0^{\pi/2} \frac{dx}{\sqrt{1 - K^2 \sin^2 x}}$

- SIMPLY, INPUT K **[D]** $\rightarrow Z(K)$

LBL d COMPUTES $Z'(K) = \int_0^{\pi/2} \frac{dx}{\sqrt{1 - (1-K^2)\sin^2 x}}$) INPUT K **[FD]** $\rightarrow Z'(K)$

CHARACTERISTICS

- IT TAKES FROM 16 TO 32 SECONDS. ABOUT 22 ON THE AVERAGE
- K MUST NOT BE $K < 10^{-4}$ (FOR $K < 10^{-4}$, $Z(K) = \pi/2$)
OR $K = 1$ (IF $K = 1$, $Z(K) = \infty$)
- USING **LBL D** OR **LBL d** DOES NOT ALTER STORED ZEROS
- ACCURACY IS 8 DECIMALS OR BETTER

LBL e STORES K FOR $SM(N, K)$ COMPUTATIONS : K **[FE]** $\rightarrow K$

LBL E COMPUTES $SM(N, K)$ • K IS ASSUMED TO BE IN RE ; N **[E]** $\rightarrow SM(N, K)$

CHARACTERISTICS

- IT TAKES 11 SECONDS
- $0 \leq K \leq$ SOME UNDEFINED VALUE
- IT DOES NOT ALTER STORED ZEROS
- ACCURACY IS 8 DECIMALS OR BETTER FOR NON-OUT OF RANGE VALUES OF K

Card 2 IS AN OPTIONAL COMPLEMENT TO CARD 1. ONCE CARD 1 HAS DETERMINED DEGREE, AND ZEROS & POLES, THE LOSS FOR ANY FREQUENCY CAN BE COMPUTED • THERE ARE SEVERAL OPTIONS:

LBL A COMPUTES THE LOSS (IN DECIBELS) FOR A GIVEN ω (NOTE = THE FIRST ω TAKES MORE TIME TO BE COMPUTED THAN ALL SUBSEQUENTS)
 ω **[A]** $\rightarrow A(\omega)$ (DSP 4)

LBL B SETS LINEAR SWEEP : **[B]** $\rightarrow 0.0000$ (LINEAR $\equiv \omega_1 = \omega_0 + \Delta$, $\omega_2 = \omega_1 + \Delta$, etc)

LBL C SETS LOGARITHMIC SWEEP : **[C]** $\rightarrow 1.0000$ (LOGARITH $\equiv \omega_1 = \omega_0 \cdot \Delta$, $\omega_2 = \omega_1 \cdot \Delta$, etc)

LBL D STARTS SWEEP : ω_0 **[ENTER]** Δ **[D]** $\rightarrow A(\omega_0)$
 $\rightarrow A(\omega_1)$
 $\rightarrow A(\omega_2)$, etc.

(LINEAR SWEEP IS SELECTED WHEN CARD 2 IS LOADED)

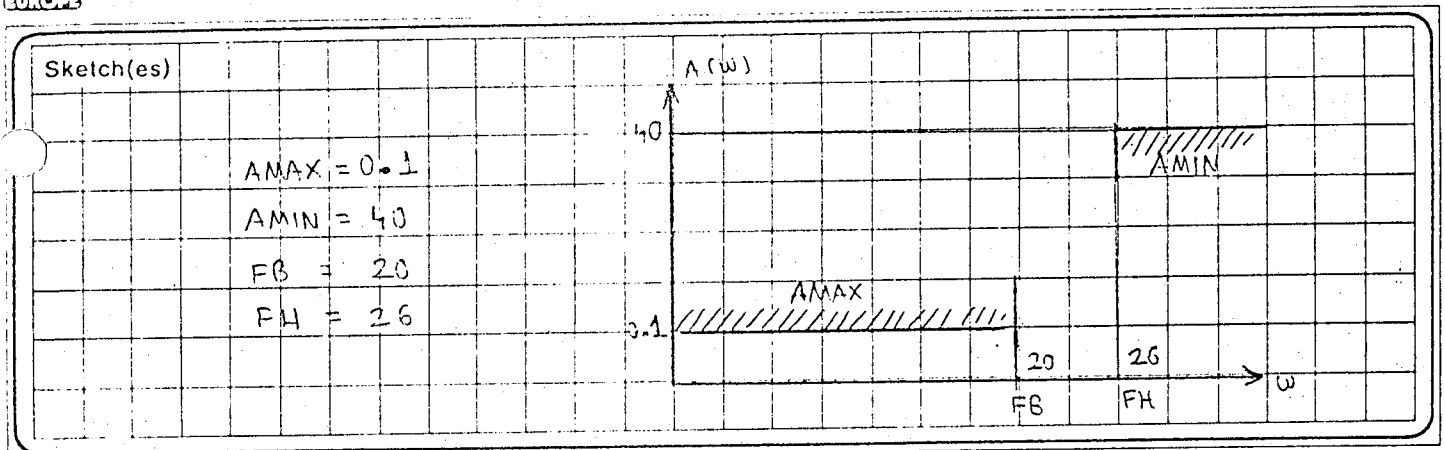
SWEEP CAN BE STOPPED BY PRESSING **[R/S]** AFTER $A(\omega_i)$ IS PRINTED.

(THIS IS, AS SOON AS THE PRINTER WORKS OR THE DISPLAY FLASHES, PRESS **[R/S]**)

(OTHERWISE, AN UNDESIRABLE **[P/S]** MAY HAVE BEEN PERFORMED.)

LBL E IS A REVIEWING ROUTINE. IT REVIEWS ZEROS & POLES (SEE **LBL C** ON CARD 1) IT'S INCLUDED TO AVOID RELOADING OF CARD 1 FOR REVIEWING PURPOSES.

Program Description II



Sample Problem(s) FIND ALL NECESSARY INFORMATION ABOUT AN ELLIPTIC LOWPASS FILTER THAT MEETS THE FOLLOWING REQUIREMENTS (SEE SKETCH)

$$A_{MAX} = 0.1 \text{ dB}, A_{MIN} = 40 \text{ dB}, FB = 20, FH = 26$$

a) DEGREE. — LOAD CARD 1, BOTH SIDES

— INPUT FILTER REQUIREMENTS: 40 [ENTER] 0.1 [ENTER] 26 [ENTER] 20 [A] → 6.00

SO, THE MINIMUM DEGREE IS 6, WE NEED A 6TH-ORDER E. LOWPASS FILTER.

b) LOSS AS A FUNCTION OF FREQUENCY

— WE WANT TO MAKE A DRAWING OF THE LOSS AS A FUNCTION OF FREQUENCY. TO OBTAIN THIS GRAPHIC, WE MUST FIND THE MOST RELEVANT ABSCISSAE:

(1) ZEROS & POLES: [R] → (1) → 6.245011340 → 82.60507346

→ (2) → 15.62227766 → 33.28579938

→ (3) → 14.56561718 → 26.57723471 → 0.00

ZEROS POLES

Solution(s)

(2) FREQUENCIES OF MAXIMUM PASSBAND LOSS

— THESE ARE $f_{pi} = FB \sin\left(\frac{2i\pi}{m}\right)$; $i = 0, 1, 2, 3$

— PROCEED AS FOLLOWS = [DSP] 6 [E] → $f_{p0} = 0.0000$

IE: $f_{p1} = 20 \sin\left[\frac{2\pi}{6}, \frac{20}{26}\right] \rightarrow$ [PCLO] 2 [X] 6 [E] 20 [X] → $f_{p1} = 11.6623$

[PCLO] 4 [X] 6 [E] 20 [X] → $f_{p2} = 18.1792$

Reference(s) (1) APPROXIMATION METHODS FOR ELECTRONIC FILTER DESIGN—

AUTHOR: RICHARD W. DANIELS — MAC GRAW-HILL BOOK COMPANY — PAGES 51 TO 82

(2) MODERN FILTER THEORY AND DESIGN

AUTHOR: EDITED BY GABOR L. TEVES & SANJIT K. MITRA — JOHN WILEY & SONS — PAGES 31 TO 53

$\boxed{RC} \boxed{E} \boxed{20} \boxed{X} \rightarrow f_{e3} = 20.0000$

(3) FREQUENCIES OF MINIMUM STOPBAND LOSS

- THESE ARE GIVEN BY $f_{ei} = \frac{FB \times FH}{f_{ei}}$

$$\left. \begin{aligned} f_{e1} &= \frac{20 \times 26}{11.6623} = 44.5881, & f_{e2} &= \frac{520}{18.1742} = 28.6041 \\ f_{e3} &= \frac{20 \times 26}{20} = 26.0000, & f_{e0} &= \frac{20 \times 26}{0} \rightarrow \infty \end{aligned} \right\}$$

- WE ARE READY FOR THE LOSS COMPUTATION - LOAD CARD Z (ITS ONLY SIDE)

- LET'S CALCULATE SOME POINTS MANUALLY

THE ZEROS = 0.2950 $\boxed{A} \rightarrow 0.0000$
 15.6223 $\boxed{A} \rightarrow 0.0000$
 19.5050 $\boxed{A} \rightarrow 0.0000$

THE F_i OF MAX. PASSBAND LOSS = 11.6623 $\boxed{A} \rightarrow 0.1000$ dB
 18.1742 $\boxed{A} \rightarrow 0.1000$ dB
 20 $\boxed{A} \rightarrow 0.1000$ dB

THE NEAR-POLES = 82.6050 $\boxed{A} \rightarrow 161.3803$ dB
 33.2857 $\boxed{A} \rightarrow 139.7303$ dB
 26.5772 $\boxed{A} \rightarrow 133.7020$ dB

THE F_i OF MIN. STOPBAND LOSS:
 44.5881 $\boxed{A} \rightarrow 46.8540$
 28.6041 $\boxed{A} \rightarrow 46.8540$
 26 $\boxed{A} \rightarrow 46.8540$
 $\infty \Rightarrow 100000 \boxed{A} \rightarrow 46.8540$

- AND, FINALLY, A GENERAL SWEEP - SELECT LINEAR SWEEP:

$\boxed{B} \rightarrow 0.0000$, 0 \boxed{ENTER} 2 $\boxed{D} \rightarrow (0.0000) \rightarrow 0.1000 \rightarrow (2.0000) \rightarrow 0.0783$
 $\rightarrow (4.0000) \rightarrow 0.0311 \rightarrow (6.0000) \rightarrow 0.0000$ --- etc

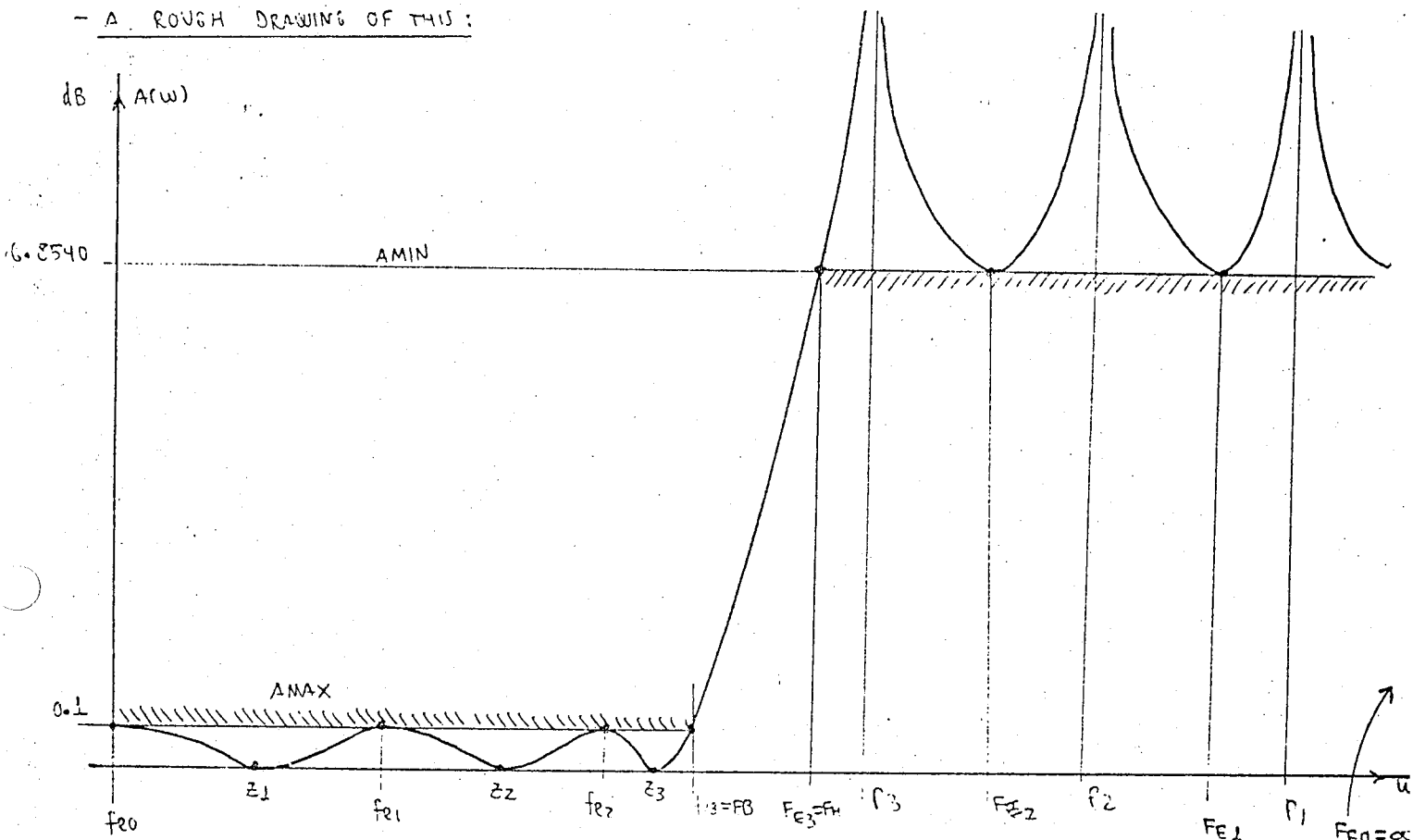
WE THUS FORM THE TABLE:

ω	0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
$A(\omega)$	0.1000	0.0783	0.0311	0.0000	0.0200	0.0748	0.0987	0.0431	0.0036	0.0980	0.1000	7.1868	24.8545	46.8540	47.3712	48.6007	56.9113	63.0148	52.7390

PASS BAND (LOSS ≤ 0.1000)

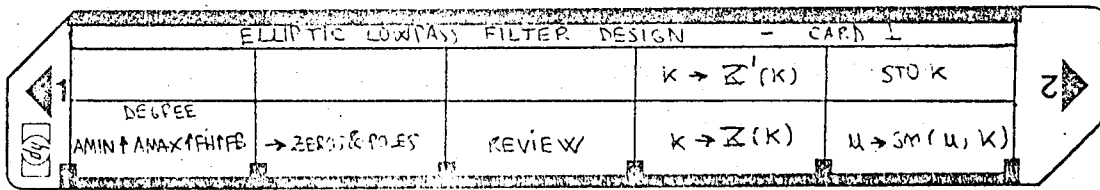
STOPBAND (LOSS ≥ 46.8540)

- A ROUGH DRAWING OF THIS:





User Instructions



STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNITS
1	LOAD CARD 1, BOTH SIDES		<input type="text"/>	
2	INPUT AMIN, AMAX, FH, FB, AND COMPUTE DEGREE m	AMIN dB AMAX dB FH Hz FB Hz	ENTER ENTER ENTER A	DEGREE m
3	OPTIONAL= FIND ZEROS & POLES		B <input type="text"/>	$\rightarrow (1) \rightarrow z_1 \rightarrow p_1$ $\rightarrow (2) \rightarrow z_2 \rightarrow p_2$ etc
4	OPTIONAL= REVIEW ZEROS & POLES		C <input type="text"/>	$\rightarrow (i) \rightarrow z_i \rightarrow p_i$ etc
5	OPTIONAL= COMPUTE $Z(K)$	K	D	$Z(K)$
6	OPTIONAL= COMPUTE $Z'(K)$	K	F D	$Z'(K)$
7	OPTIONAL= COMPUTE $S_m(u, K)$	K u	F E E	K $S_m(u, K)$
8	OPTIONAL= LOAD CARD 2, SIDE 1			
9	TO COMPUTE THE LOSS AT SOME FREQUENCY ω	ω Hz	A	$A(\omega)$ dB
10	TO PERFORM A SWEEP OF FREQUENCIES:			
	a) SELECT LINEAR OR		B	0.0000
	b) SELECT LOGARITHMIC MODE		C	1.0000
	START SWEEP:	ω_0 Hz	ENTER	
		Δ	D	$\rightarrow (\omega_i) \rightarrow A(\omega_i)$ etc
	TO STOP SWEEP, PRESS [R/S] AFTER $A(\omega_i)$			
11	TO REVIEW ZEROS AND POLES		E	$\rightarrow (i) \rightarrow z_i \rightarrow p_i$ etc.
12	FOR ANOTHER CASE, GO TO APPROPRIATE STEP.			
CARD 2				
ELLIPTIC LOWPASS FILTER DESIGN - CARD 2 -				
1	$\omega \rightarrow A(\omega)$	LINEAR	SWEEP LOGARITHMIC	$\omega_0 \Delta \rightarrow A(\omega_i)$
			REVIEW	

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	* LBLA	31 25 11	DEGREE COMPUTATION		SIN	31 62	$\sqrt{1-x^2}$ $1 + \sin(\cos^{-1} x)$ NEW $\phi_i \rightarrow \phi_{i+1}$ $\phi_i \rightarrow \phi_{i+1}$ NEW $x_i \rightarrow x_{i+1}$ $x_{i+1} = 0?$ NO, ITERATE YES:
	STOD	33 14	STORES FB		STI	35 33	
	X=Y	35 52		060	ISZ	31 34	
	÷	81			RCL7	34 07	
	STOE	33 15	STORES $K = 1/x_L$		SIN	31 62	
	R↓	35 53			X	71	
	GSB8	31 22 08	COMPUTES E		SIN ⁻¹	32 62	
	STOA	33 11	STORES E		STO+7	33 61 07	
	X≥Y	35 52			Z	02	
010	GSB8	31 22 08	COMPUTES $\frac{1}{L}$ COMP. & STORES $R(\frac{1}{L})$ COMP. $R'(1/x_L)/R'(1/L)$ $m = \left[\frac{R(\frac{1}{x_L}) \cdot R'(\frac{1}{L})}{R'(\frac{1}{x_L}) \cdot R(\frac{1}{L})} \right] + 1$		STO=7	33 81 07	
	÷	81				RCL	35 34
	√	31 54				÷	81
	GSB9	31 22 09			070	STOX8	33 71 08
	STOC	33 13				↓	01
	RCLC	34 15				-	51
	GSB9	31 22 09				STO9	33 09
	RCLC	34 13				X≠0	31 61
	÷	81				STO3	22 03
	↓	01				RCL7	34 07
220	+	61			Z	02	
	INT	31 33			÷	81	
	STOC	33 13			↓	01	
	RTN	35 22			TAN ⁻¹	32 64	
	* LBL8	31 25 08	AUXILIAR SUBROUTINE	080	+	61	
	.	83			TAN	31 64	
	↓	01	COMPUTES EITHER		LN	31 52	
	X	71	0.1 AMAX		RCL8	34 08	
	10 ^x	32 53	10 - 1		X	71	
	↓	01	OR		P≥S	31 42	
	-	51	0.1 AMIN - 1		RTN	35 22	
330	RTN	35 22			* LBLB	31 25 12	
	* LBL9	31 25 09	AUXILIAR SUBROUTINE		CFO	35 61 08	
	STO9	33 09			RCLC	34 13	
	GSBD	31 22 14	$R(\frac{1}{x_L})$ OR $R(\frac{1}{L})$	090	Z	02	
	STO8	33 08			÷	81	
	STO0	33 00			ENTER↑	41	
	RCL9	34 09			INT	31 83	
	GSBd	32 22 14	$R'(\frac{1}{x_L})$ OR $R'(\frac{1}{L})$		STOB	33 12	
	STO=8	33 81 08			STI	35 33	
410	RCL8	34 08	$R(\frac{1}{L})/R'(\frac{1}{L})$ OR ---		X=Y	32 51	
	RTN	35 22			SFO	35 51 00	
	* LBLD	31 25 14	R(K) COMPUTATION		* LBLC	31 25 06	
	P≥S	31 42			RCL	35 34	
	SIN ⁻¹	32 62	$\sqrt{1-x^2}$	100	Z	02	
	COS	31 63				X	71
	P≥S	31 42				0	00
	* LBLd	32 25 14		R'(K) COMPUTATION		F0?	35 71 00
	P≥S	31 42			2 ^x	32 52	
	STO9	33 09	STORE X0		-	51	
550	↓	01			RCLC	34 13	
	STO8	33 08	STORE P0		÷	81	
	SIN ⁻¹	32 62	STORE Q0 = $\pi/2$		RCL0	34 00	
	STO7	33 07				X	71
	RCL9	34 09		RCL X0	110	GSRE	31 22 15
	* LBL3	31 25 03	LOOP		RCLD	34 14	
	COS ⁻¹	32 63			X	71	

REGISTERS

0	1	2	3	4	5	6	7	8	9
$R(\frac{1}{L})$	Z1	Z2	Z3	Z4	Z5	Z6	Z7	used, Z8	used, Z9
10	11	12	13	14	15	used	used	used	used
Z10	Z11	Z12	Z13	Z14	Z15	used	used	used	used
E, used	B	C	D	E	F	G	H	I	J
	AMIN, INT(m ₂), x ₀	m	FB	$K = \frac{1}{x_L}$	used				



Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
	STO(i)	33 24	STORE X2i		N!	35 81	$sm(u, x) = \frac{u}{8} -$ $-(1+k^2 \times u/8)^3 +$ $\frac{3!}{3!} +$ $+ (1+14k^2 + k^4) \times (u/8)^5 +$ $\frac{5!}{5!} + \dots$
	DSZ	31 33		170	STOG	33 06	
	GTO 6	22 06	LOOP		X	71	
	*LBLC	31 25 13	DISPLAY & REVIEW ROUTINE		+	61	
	0	00	RESET INDEX TO 0		X	71	
	STI	35 53			7	07	
	*LBL0	31 25 00	LOOP		N!	35 81	
120	ISZ	31 34			÷	81	
	RCL	35 54			X	71	
	DSPO	23 00	} DISPLAY i		RCL7	34 07	
	PAUSE	35 72				RCL6	34 06
	DSP9	23 09			180	÷	81
	RCLD	34 14				-	51
	X ²	32 54			X	71	
	RCL(i)	34 24			X	71	
	-X-	31 84	DISPLAY X2i		RCL8	34 08	
	RCL E	34 15	} COMPUTE Xpi		G	06	
130	X	71				÷	81
	÷	81			+	61	
	-X-	31 84	DISPLAY Xpi		X	71	
	RCLB	34 12	} ALL DISPLAYED?		X	71	
	RCL I	35 34			190	÷	01
	X≠Y	32 61				-	51
	GTO 0	22 00	NO REPEAT		X	71	
	CLX	44	YES, RESET		CHS	42	
	DSPZ	23 02			*LBL4	31 25 04	DUPLICATION FORMULA
	RTN	35 22			STOG	33 06	
140	*LBLR	32 25 15	STORE X		STOXG	33 71 06	
	STOE	33 15			2	02	
	RTN	35 22			X	71	
	*LBL E	31 25 15	SM(u, x) COMPUTATION		L	01	
	P≥S	31 42		200	RCLG	34 06	
	SF3	35 51 03			OSB7	31 22 07	
	SF2	35 51 02			OSB7	31 22 07	
	8	08	u → u/8		-	51	
	÷	81			÷	81	
	RCL E	34 15			F2?	35 71 02	
150	X ²	32 54			CTO4	22 04	DUPLICATE AGAIN
	STO9	33 09			F3?	35 71 03	
	STO7	33 07			CTO4	22 04	DUPLICATE ONCE MORE
	STOG	33 06			P≥S	31 42	
	I	01		210	RTN	35 22	
	+	61	sm(u, x) is		*LBL7	31 25 07	AUXILIAR SUBROUTINE
	STO8	33 08	APPROXIMATED		-	51	
	STOXG	33 71 06	BY A		√	31 54	
	X ²	32 54	TAYLOR'S		X	71	
	RCL7	34 07	SERIES		1	01	
160	I	01	EXPANSION		RCL9	34 09	
	2	02			RCLG	34 06	
	X	71			STOXG	33 71 06	
	+	61			X	71	
	STO7	33 07		220	RTN	35 22	
	RCL8	34 08					
	X	71					
	RCLG	34 06					
	5	05					

LABELS					FLAGS		SET STATUS			
A DEGREE	B → ZEROS, POL.	C REVIEW	D X → Z'(X)	E u → sm(u, x)	0 ODD/EVEN	FLAGS			TRIG	DISP
a	b	c	d x → Z'(x)	e STO X	1	ON OFF			DEG	FIX
0 used REVIEW	1	2	3 used Z'(x)	4 used sm(u, x)	2 used sm(u, x)	0	<input type="checkbox"/>	<input checked="" type="checkbox"/>	GRAD	SCI
5	6 used Z, P	7 used sm(u, x)	8 used DEGREE	9 used DEGREE	3 used sm(u, x)	1	<input type="checkbox"/>	<input checked="" type="checkbox"/>	RAD	ENG
						2	<input type="checkbox"/>	<input checked="" type="checkbox"/>		n
						3	<input type="checkbox"/>	<input checked="" type="checkbox"/>		

HP47 OWNERS: USE THOSE 4 FREE STEPS TO INSERT "SPACE" AND CHANGE "PAUSE" TO "PRINT X"

DON'T FORGET.

